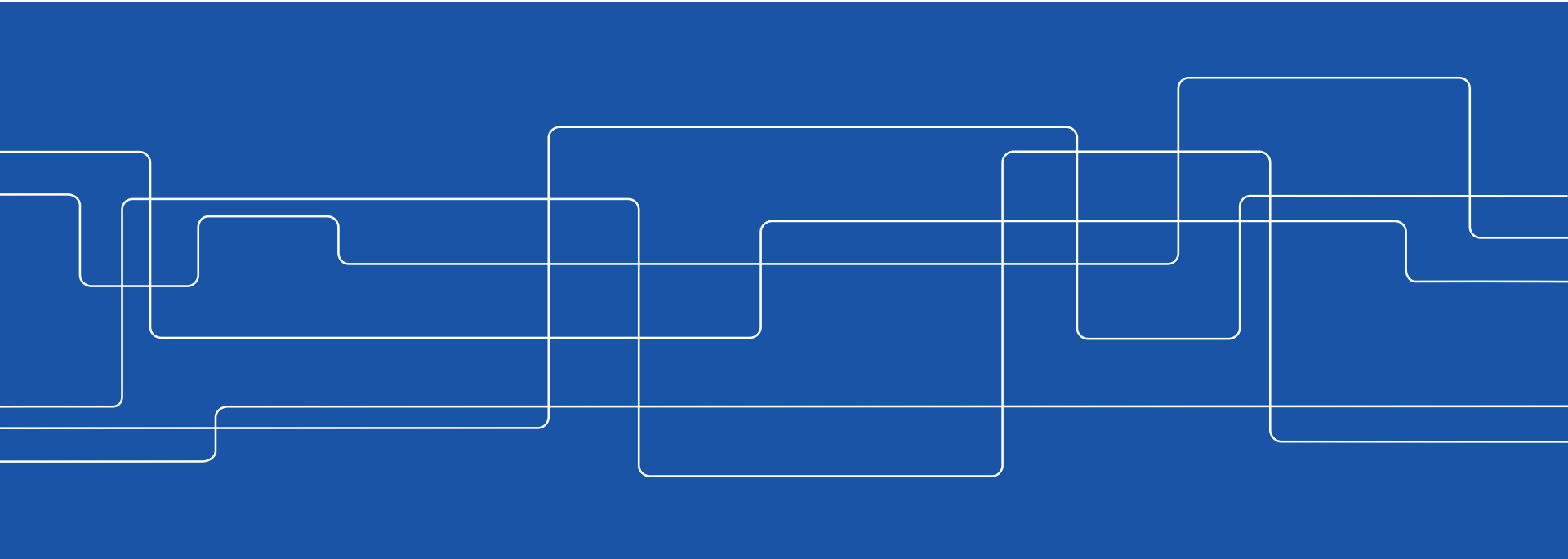




# MERiT

MEthane in Rocket nozzle cooling channels -  
conjugate heat Transfer measurements

Jens Fridh (KTH) / Jan Östlund (GKN), NRFP3 seminar - 15 Nov 2018



# Background (1/3)

- Propulsion system using hydrocarbons (Methane)
  - grand challenge for today's rocket and space propulsion systems
  - Possibility for re-fueling @ extraterrestrial territories with local assets of Methane (Mars... H<sub>2</sub>O CO<sub>2</sub>)
  - Good performance indicators
    - Reasonably good specific thrust (~380 s @ sea level)
    - Good storage stability, cooling capabilities and availability
    - Low toxicity and production cost



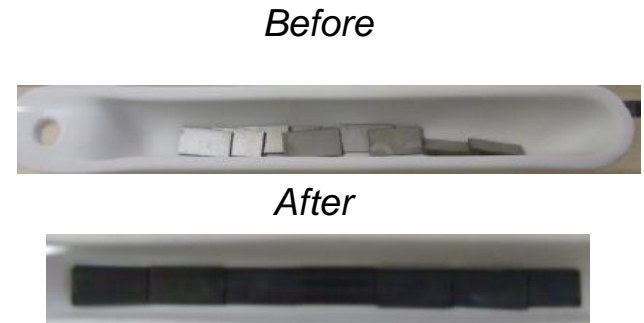
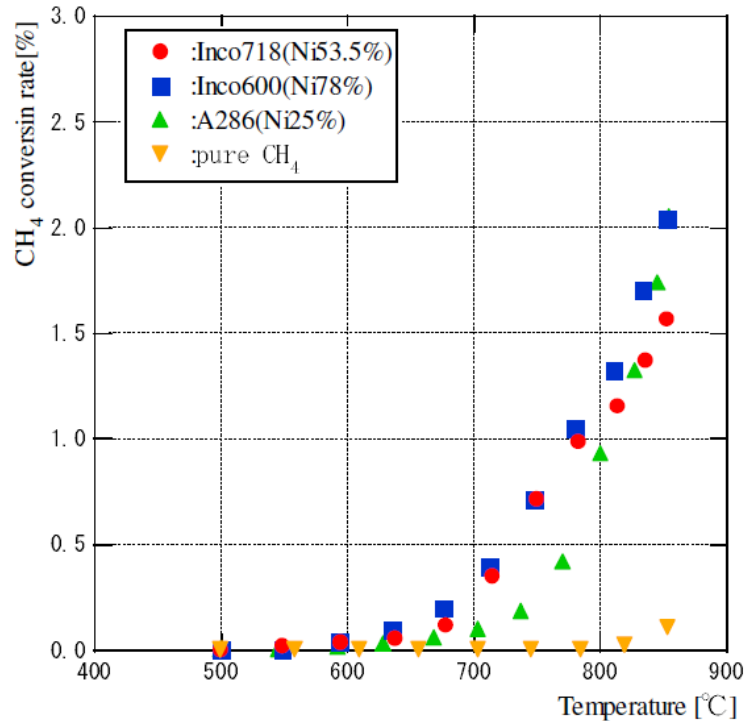
*SpaceX  
Raptor Engine  
Engine tests Sep-16*



## Background (2/3)

- Rocket nozzle challenges
  - Coking in cooling channels due to fuel impurities and/or from thermal decomposition of methane @ high temperatures
  - Degradation of the heat transfer capabilities
  - Increased cooling channel pressure losses
- It is of utter importance for future nozzle designs to quantify the heat transfer characteristics of typical Nickel-based alloy steels used, e.g. 21-6-9
- Very few places in the world having the infrastructure for heat transfer studies of this type

# Background (3/3)



**Reference:**  
Kazuyuki Higashino et al., AIAA 2008-4753

(d) The sweep of temperature experiment increase  
Fig.2. Experimental results of CH<sub>4</sub> thermal cracking(Ni contents of each material mass level is shown)



# Project Objectives

- For a relevant alloy (21-6-9) and typical cooling channel geometries, fuel grade and operating conditions determine:
  - heat transfer coefficient
  - degree of coking and corrosion
  - pressure loss

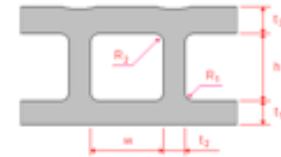
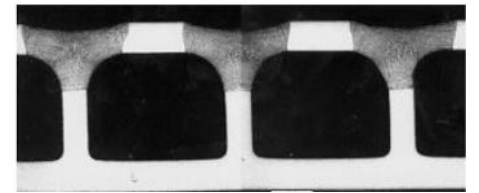
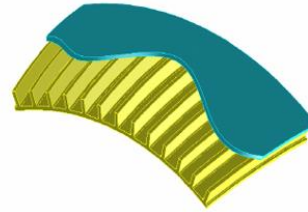
as a function of

- heat load
- wall temperature
- Reynolds number
- fuel grade
- pressure level

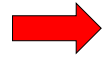
## Methodology

- Design and commission a test rig for conjugate heat transfer studies according to specs and perform trials
- Supported with numerical studies

# Specifications



#	Material	Heat flux (MW/m <sup>2</sup> )	Pressure level (bar)	Inlet temperature (K)	w (-)	h (-)	t <sub>1</sub> (-)	t <sub>2</sub> (-)	t <sub>3</sub> (-)	Length (-)
1	21-6-9 Carpenter 40	~6...7	40...160	270...655	0.16	0.16	0.06	0.1	0.08	0.75
2	21-6-9 Carpenter 40	~3.5...4.5	40...160	270...655	0.16	0.26	0.06	0.1	0.08	1
3	21-6-9 Carpenter 40	~1...2	40...160	270...655	0.3	0.26	0.06	0.1	0.08	1
4	Inco600	~6...7	40 bar	270...655	0.28	0.48	0.06	0.06	0.06	1



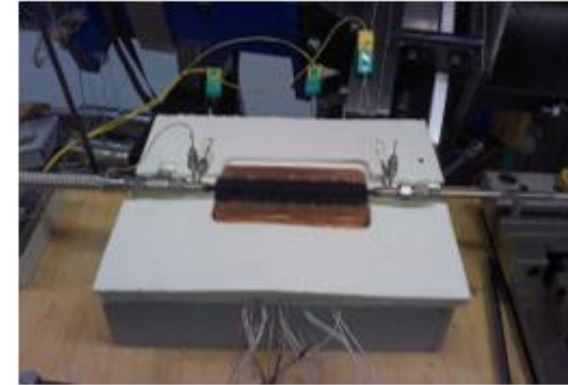
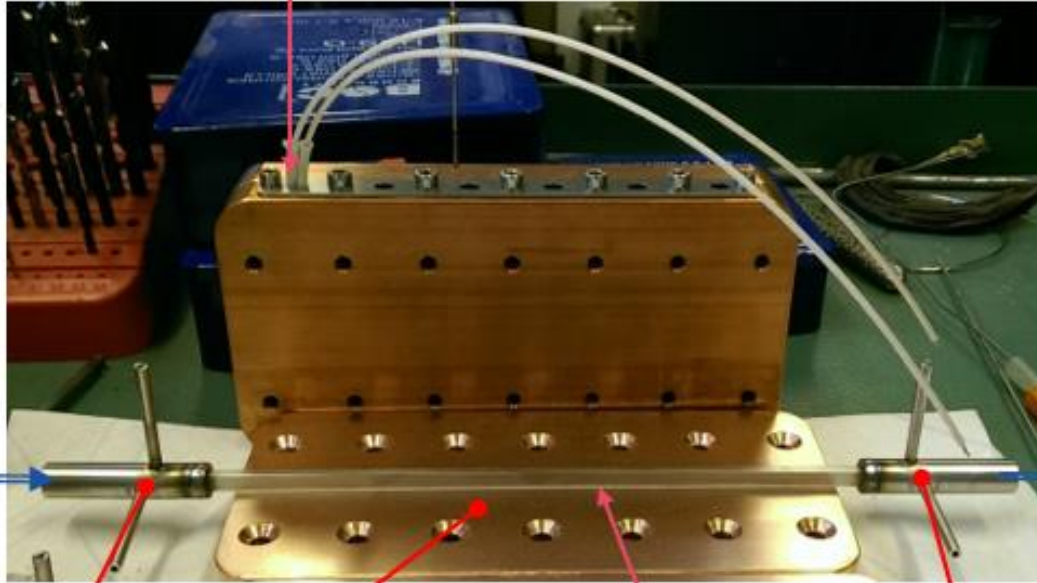
- Channel outlet temperature: < 800 K

# MERiT - Project plan

NRFP 3 - MERiT										Today	
Work packages	Description	<div style="display: flex; justify-content: space-between;"> <span>20160901 - 20161130</span> <span>20161201 - 20170228</span> <span>20170301 - 20170531</span> <span>20170601 - 20170831</span> <span>20170901 - 20171130</span> <span>20180301 - 20180228</span> <span>20180501 - 20180531</span> <span>20180901 - 20181230</span> </div>								share	
WP 0	Project lead	■	■	■	■	■	■	■	■	■	5%
WP 1	Conceptual study & heater tests	■	■	■						■	10%
WP 2	Design test rig		■	■	■	■					20%
WP 3	Infrastructure, risk assesment	■	■	■	■	■	■	■	■	■	20%
WP 4	Commissioning test rig				■	■	■	■	■	■	10%
WP 5	Test campaign				■	■	■	■	■	■	25%
WP 6	Synthesis of results							■	■	■	10%
<b>Deliverables</b>											Responsibility
D 0	Reference group meetings, minutes	x	x	x	x	x	x	x	x	x	GKN
D 1.1	Report – conceptual study	■	■								KTH
D 1.2	Report – heater tests		■								KTH
D 2	MSc thesis (optional)			■							GKN
D 3	Test facility installed, risk assessment report			■	■	■	■	■	■	■	KTH
D 4	Technical report, commissioning					■	■	■	■	■	KTH
D 5.1	Test & measurement plan				■	■	■	■	■	■	KTH
D 5.2	MSc thesis (optional), internship					■	■	■	■	■	GKN
D 5.3	MSc thesis (optional), internship							■	■	■	KTH
D 6.1	Technical report, test campaign							■	■	■	KTH
D 6.2	International paper, results						■	■	■	■	KTH/GKN
D 6.3	Final report, technical/economical							■	■	■	KTH/GKN

# WP1: Inert (air) tests – Inco600 (4x6x180, t0.6)

6 x 400W heater cartridges,  $T_4$  (heater pin)



$T_1$  (bulk-inlet)

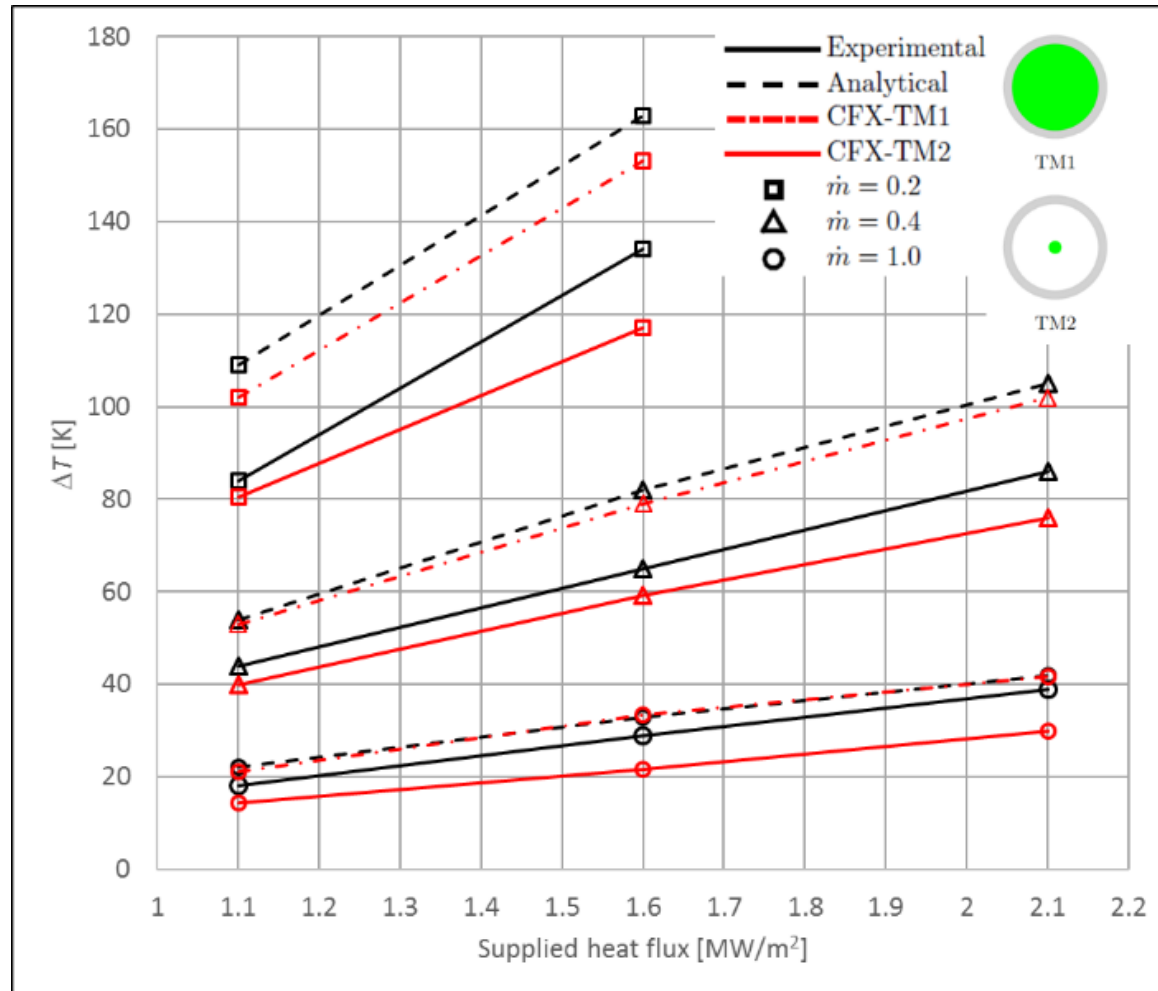
$T_2$  (Cu-block)

Soldered (Au alloy – melt-point 1350 K)

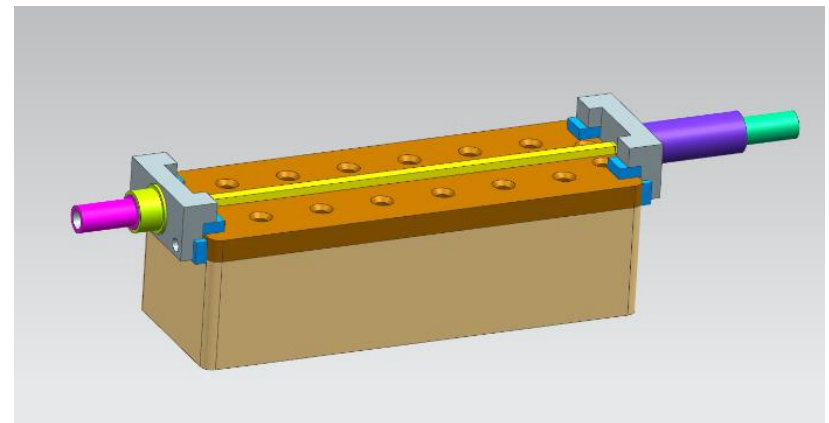
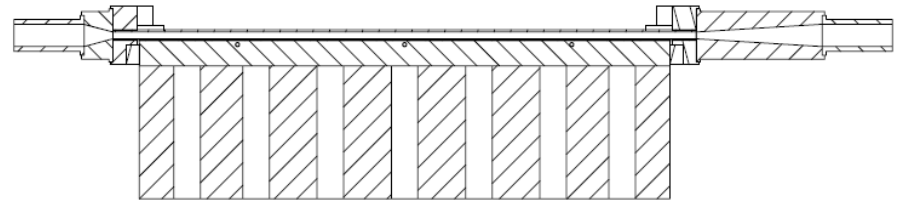
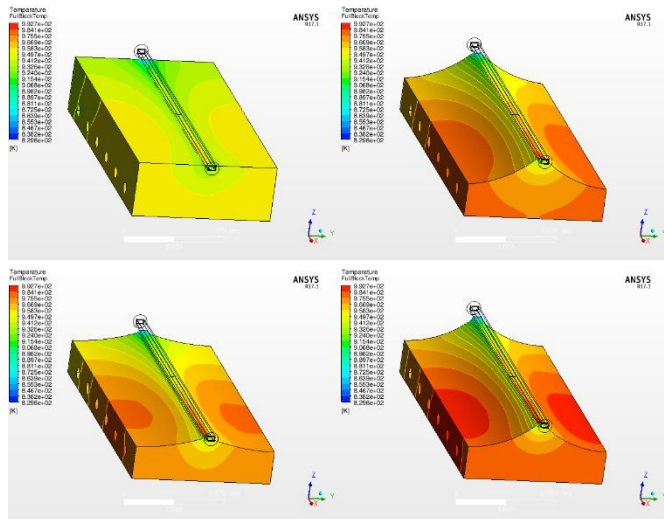
$T_3$  (bulk-outlet)



# WP1: heater trials EXP / 1D / 3D CFD



# Final Heater Design (WP2)



## Targets:

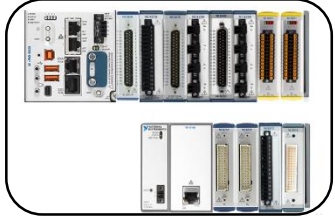
Maximize the heat pick-up

Minimize the maximum block-temperature

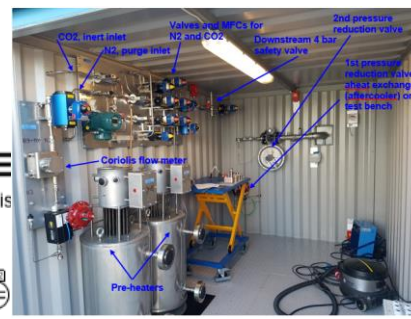


# Infrastruktur (WP3)

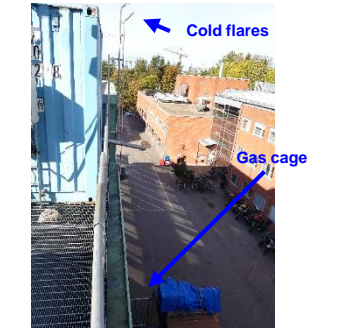
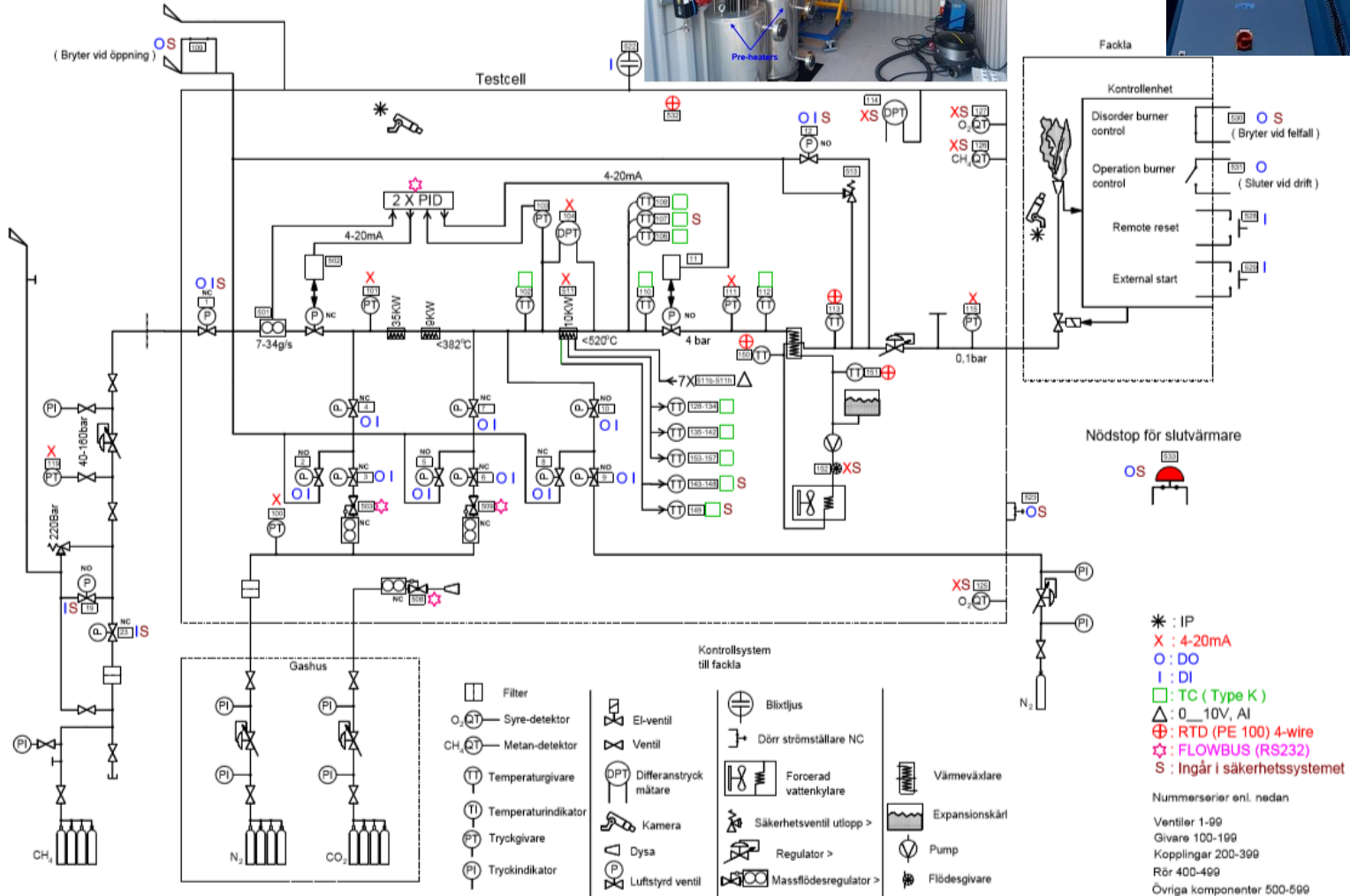
NI cRIO: Control & Measurement system



ME Systemskis

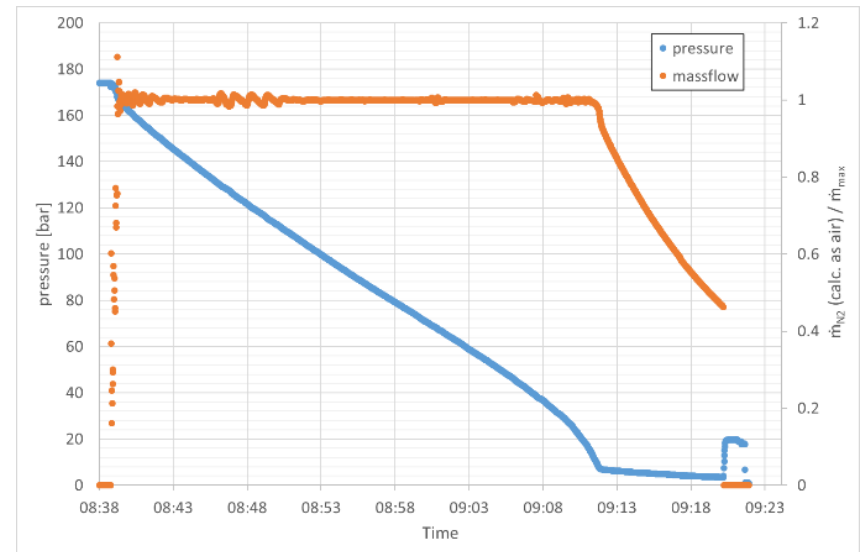


Fackla



# Commissioning (WP4)

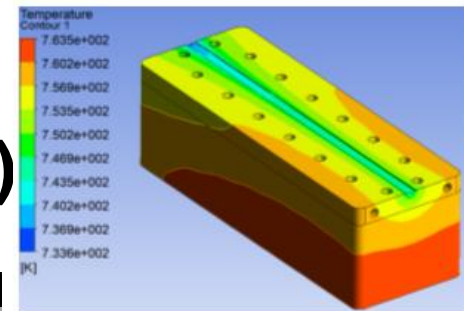
- Risk assessment
- Gas supply system
  - April 2017
- Flare system
  - Dec 2017
- Process
  - ....



# Test plan preliminary trials (WP5)

Limited due to economical and time restrictions

Test ID	channel #	q (MW/m <sup>2</sup> )	PTI (bar)	TTI (nor)	m (-)	DPT_est (norm)		TTO_est (norm)		MO_est (norm)	
						1D	CFD	1D	CFD	1D	CFD
D301	3	1,5	40	0,687	low	0,008	0,012	0,654	0,659	0,2	0,22
D302	3	1,5	100	0,687	low	0,003	0,005	0,651	0,655	0,08	0,08
D303	3	1,5	160	0,687	low	0,002	0,003	0,650	0,653	0,05	0,052
D304	3	1,5	40	1	medium	0,092	0,144	0,845	0,856	0,8	0,76
D305	3	1,5	100	1	medium	0,038	0,056	0,845	0,848	0,28	0,28
D306	3	1,5	160	1	medium	0,024	0,036	0,844	0,846	0,18	0,18
D307	3	1,5	60	1	high	0,178	0,284	0,834	0,849	0,92	0,9
D308	3	1,5	100	1	high	0,108	0,164	0,834	0,839	0,5	0,5
D309	3	1,5	160	1	high	0,068	0,104	0,834	0,836	0,3	0,3
<del>D201</del>	<del>2</del>	<del>3,5</del>	<del>40</del>	<del>0,5344</del>	<del>low</del>	<del>0,032</del>	<del></del>	<del>0,604</del>	<del></del>	<del>0,4</del>	<del></del>
<del>D202</del>	<del>2</del>	<del>3,5</del>	<del>100</del>	<del>0,5344</del>	<del>low</del>	<del>0,012</del>	<del></del>	<del>0,594</del>	<del></del>	<del>0,14</del>	<del></del>
<del>D203</del>	<del>2</del>	<del>3,5</del>	<del>160</del>	<del>0,5344</del>	<del>low</del>	<del>0,008</del>	<del></del>	<del>0,588</del>	<del></del>	<del>0,08</del>	<del></del>
<del>D204</del>	<del>2</del>	<del>3,5</del>	<del>60</del>	<del>0,687</del>	<del>medium</del>	<del>0,224</del>	<del></del>	<del>0,615</del>	<del></del>	<del>0,88</del>	<del></del>
<del>D205</del>	<del>2</del>	<del>3,5</del>	<del>100</del>	<del>0,687</del>	<del>medium</del>	<del>0,134</del>	<del></del>	<del>0,615</del>	<del></del>	<del>0,46</del>	<del></del>
<del>D206</del>	<del>2</del>	<del>3,5</del>	<del>160</del>	<del>0,687</del>	<del>medium</del>	<del>0,084</del>	<del></del>	<del>0,614</del>	<del></del>	<del>0,26</del>	<del></del>
<del>D207</del>	<del>2</del>	<del>3,5</del>	<del>80</del>	<del>0,7634</del>	<del>high</del>	<del>0,546</del>	<del></del>	<del>0,653</del>	<del></del>	<del>1,46</del>	<del></del>
<del>D208</del>	<del>2</del>	<del>3,5</del>	<del>120</del>	<del>0,7634</del>	<del>high</del>	<del>0,366</del>	<del></del>	<del>0,653</del>	<del></del>	<del>0,74</del>	<del></del>
<del>D209</del>	<del>2</del>	<del>3,5</del>	<del>160</del>	<del>0,7634</del>	<del>high</del>	<del>0,278</del>	<del></del>	<del>0,653</del>	<del></del>	<del>0,52</del>	<del></del>
<del>D101</del>	<del>1</del>	<del>4</del>	<del>40</del>	<del>0,458</del>	<del>low</del>	<del>0,068</del>	<del></del>	<del>0,525</del>	<del></del>	<del>0,6</del>	<del></del>
<del>D102</del>	<del>1</del>	<del>4,5</del>	<del>100</del>	<del>0,458</del>	<del>low</del>	<del>0,024</del>	<del></del>	<del>0,528</del>	<del></del>	<del>0,22</del>	<del></del>
<del>D103</del>	<del>1</del>	<del>4,5</del>	<del>160</del>	<del>0,458</del>	<del>low</del>	<del>0,014</del>	<del></del>	<del>0,515</del>	<del></del>	<del>0,12</del>	<del></del>
<del>D104</del>	<del>1</del>	<del>6</del>	<del>60</del>	<del>0,458</del>	<del>medium</del>	<del>0,354</del>	<del></del>	<del>0,446</del>	<del></del>	<del>1,36</del>	<del></del>
<del>D105</del>	<del>1</del>	<del>6</del>	<del>100</del>	<del>0,458</del>	<del>medium</del>	<del>0,2</del>	<del></del>	<del>0,443</del>	<del></del>	<del>0,62</del>	<del></del>
<del>D106</del>	<del>1</del>	<del>6</del>	<del>160</del>	<del>0,458</del>	<del>medium</del>	<del>0,12</del>	<del></del>	<del>0,438</del>	<del></del>	<del>0,34</del>	<del></del>
<del>D107</del>	<del>1</del>	<del>7</del>	<del>100</del>	<del>0,458</del>	<del>high</del>	<del>0,58</del>	<del></del>	<del>0,413</del>	<del></del>	<del>1,28</del>	<del></del>
<del>D108</del>	<del>1</del>	<del>7</del>	<del>130</del>	<del>0,458</del>	<del>high</del>	<del>0,44</del>	<del></del>	<del>0,414</del>	<del></del>	<del>0,8</del>	<del></del>
<del>D109</del>	<del>1</del>	<del>7</del>	<del>160</del>	<del>0,458</del>	<del>high</del>	<del>0,35</del>	<del></del>	<del>0,414</del>	<del></del>	<del>0,6</del>	<del></del>



20g 655K 40bar Configuration 3

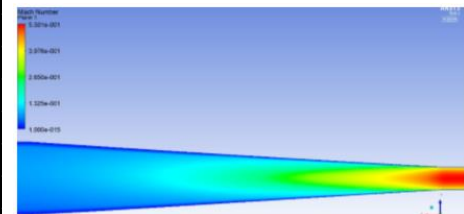
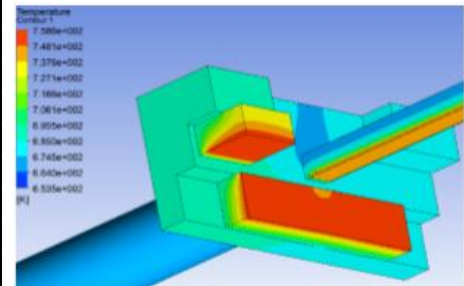


Figure 17 Outlet Mach number map in high velocity configuration

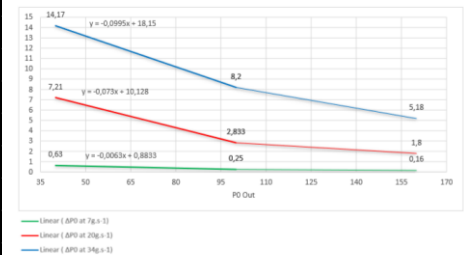
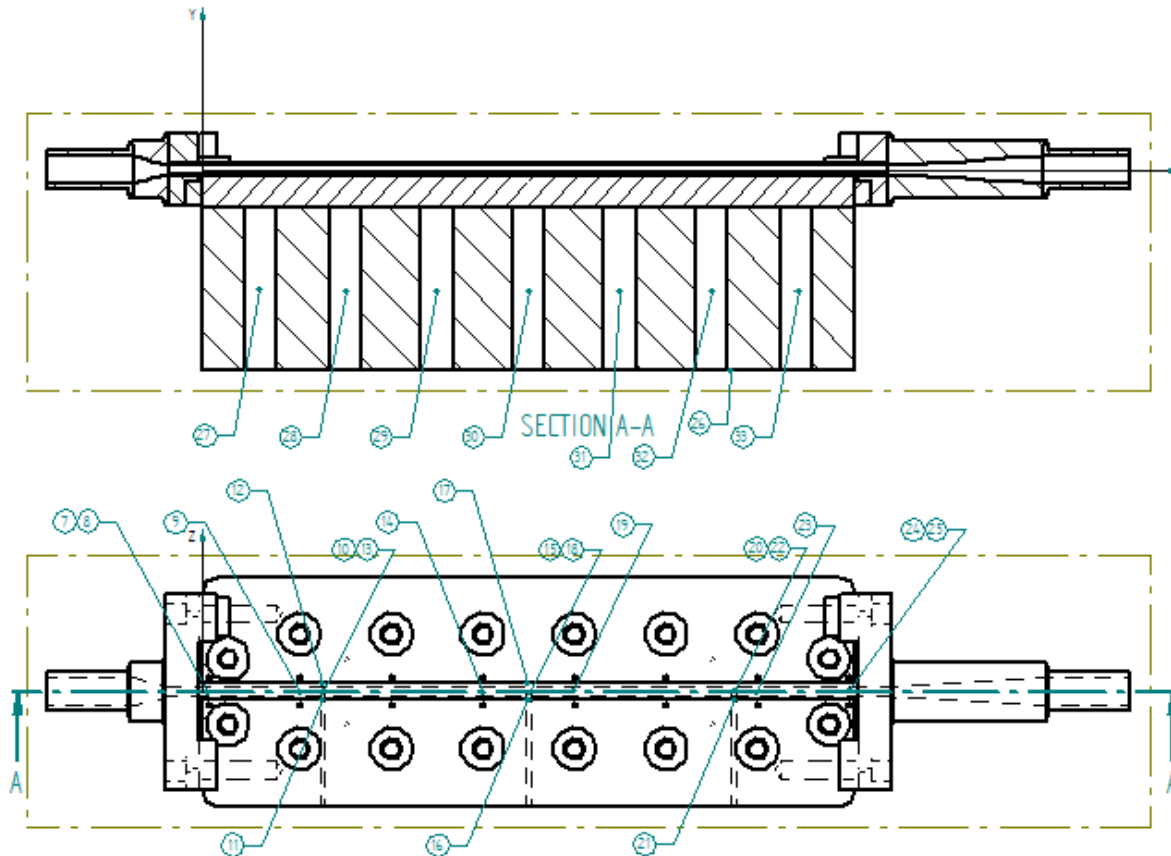


Figure 19 Pressure loss as a function of back pressure with constant mass flow rate

# Test Measurement points



Heat transfer:  
TC measurements

#	Point ID	X	Y	Z	Signal ID	Description	Note
1	TC1	0	0	0	TC1	Total Temperature inlet	Temperature chart for the action
2	TC2	0	0	0	TC2	Total Temperature inlet	Temperature chart for the action
3	TC3	0	0	0	TC3	Total Temperature inlet	Temperature chart for the action
4	TC4	0	0	0	TC4	Total Temperature inlet	Temperature chart for the action
5	TC5	0	0	0	TC5	Total Temperature inlet	Temperature chart for the action
6	TC6	0	0	0	TC6	Total Temperature inlet	Temperature chart for the action
7	TC7	0	0	0	TC7	Total Temperature inlet	Temperature chart for the action
8	TC8	0	0	0	TC8	Total Temperature inlet	Temperature chart for the action
9	TC9	0	0	0	TC9	Total Temperature inlet	Temperature chart for the action
10	TC10	0	0	0	TC10	Total Temperature inlet	Temperature chart for the action
11	TC11	0	0	0	TC11	Temperature in wall face	
12	TC12	0	0	0	TC12	Temperature in wall face	
13	TC13	0	0	0	TC13	Temperature in wall face	
14	TC14	0	0	0	TC14	Temperature in wall face	
15	TC15	0	0	0	TC15	Temperature in wall face	
16	TC16	0	0	0	TC16	Temperature in wall face	
17	TC17	0	0	0	TC17	Temperature in wall face	
18	TC18	0	0	0	TC18	Temperature in wall face	
19	TC19	0	0	0	TC19	Temperature in wall face	
20	TC20	0	0	0	TC20	Temperature in wall face	
21	TC21	0	0	0	TC21	Temperature in wall face	
22	TC22	0	0	0	TC22	Temperature in wall face	
23	TC23	0	0	0	TC23	Temperature in wall face	
24	TC24	0	0	0	TC24	Temperature in wall face	
25	TC25	0	0	0	TC25	Temperature in wall face	
26	TC26	0	0	0	TC26	Temperature in wall face	
27	TC27	0	0	0	TC27	Temperature in wall face	
28	TC28	0	0	0	TC28	Temperature in wall face	
29	TC29	0	0	0	TC29	Temperature in wall face	
30	TC30	0	0	0	TC30	Temperature in wall face	
31	TC31	0	0	0	TC31	Temperature in wall face	
32	TC32	0	0	0	TC32	Temperature in wall face	
33	TC33	0	0	0	TC33	Temperature in wall face	
34	TC34	0	0	0	TC34	Temperature in wall face	
35	TC35	0	0	0	TC35	Temperature in wall face	
36	TC36	0	0	0	TC36	Temperature in wall face	
37	TC37	0	0	0	TC37	Temperature in wall face	
38	TC38	0	0	0	TC38	Temperature in wall face	
39	TC39	0	0	0	TC39	Temperature in wall face	
40	TC40	0	0	0	TC40	Temperature in wall face	



# Outcomes...up until 2018-11-15

- Test build design
  - Conceptual and design report
  - 1 MSc thesis (NUM)
- Infrastructure design
  - Risk assessment report
  - 2 Internships (EXP, NUM)
  - Third party audit documentation
- Commissioning and Trials
  - Test and measurement plan report
- Conf.paper (SP2018)



# Summary / Outlook

## Summary

- A world-unique test rig for high pressure (200 bar), high temperature (800 K / 1023 K) and fuel thermal power < 1.8 MW heat transfer studies for channels have been designed, manufactured, installed...partly verified & commissioned
- Tight time plan to build a very complex infrastructure (high press, high temp.) → 6-8 months delay compared to the original plan → unrealistic to manage first base trials with CH<sub>4</sub> before 2019
- Acknowledgements to project funding organizations:
  - Rymdstyrelsen (NRFP3)
  - ESA (FLPP)
  - KTH, EGI Dept.(KTH)

## Outlook

- Nov-Dec 2018 – Infrastructure installed
- Dec 2018...Jan 2019 – Commissioning, Inspection, authority clearance

